



Development of a Field Laboratory for Monitoring of Fecal-Sludge Treatment Plants

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Abstract: In urban humanitarian-aid operations, safe treatment of fecal sludge is highly important. While currently field-deployable fecal-sludge treatment plants are being developed, field-ready analytical equipment for process-control and public health monitoring is missing. Within the Microbial Sludge Quality project, a field laboratory was developed. A minimum set of parameters for the considered processes was developed through literature research. The analytical methods were tested on their field applicability and, if necessary, modified. The following methods were modified for field use: bacteriological analysis (sample homogenization and counting), chemical oxygen demand (sample digestion), volatile fatty acid–alkalinity titration (redesigned test setup), total solids (redesigned test setup), and ammonia determination (redesigned test setup). For bacteriological analysis, chemical oxygen demand, and total solids the modifications lead to highly comparable analytical results. The results obtained by the field methodology for volatile fatty acid–alkalinity titration and ammonia determination were sufficient for field-process monitoring; however, they did not correlate as well. To enable rapid startup of the laboratory during humanitarian-aid missions, it was developed to include analytical and support equipment. The usage of the developed laboratory should allow close-in-time process monitoring and public-health assessments of fecal-sludge treatment plants.

Keywords: fecal-sludge treatment plant; field laboratory; process monitoring; public-health monitoring

1. Introduction

In urban or camp humanitarian-aid settings, fecal-sludge (FS) treatment is of utmost importance [1,2]. Regarding the public-health aspect, the 2010 cholera outbreak in Haiti [3] can be considered as one of the worst examples of failed fecal-sludge treatment. The impact of untreated fecal sludge released in the environment is quite dramatic and may result in algae blooms, pest problems, and overfertilization of fields. FS-treatment processes, decision-making tools for field use in humanitarian aid are currently being developed [2,4,5]. The importance of the regular monitoring of FS treatment plants is stressed in the literature [6,7]. However, due to the inhomogeneity of the samples and often inconsistency of the influent load, a publication on the characterization of fecal sludge, including analytical methods and equipment in developing countries, was published by the Swiss Federal Institute of Aquatic Science and Technology [8]. However, field-ready analytical equipment for process and public-health monitoring was found missing.



To close this gap, the Microbial Sludge Quality project (November 2016–October 2017) was funded by the Humanitarian Innovation Fund to develop a field lab for the public-health and process monitoring of field FS treatment plants.

Humanitarian-aid organizations were defined as the primary target group. During the project duration, a secondary target group consisting of social enterprises, development-cooperation organizations and local utility operators were established. Together with the Austrian Red Cross, as the project consortium's humanitarian-aid organization, and its contacts in the emergency WASH community, the following design criteria for the field laboratory were developed:

- Appropriateness: the analytical results are comparable to a fixed laboratory
- Applicability: the laboratory must work in the field
- Affordability: the laboratory has to be more cost-effective than standard solutions
- Mobility: the laboratory has to fit in a Toyota Landcruiser

These design criteria were translated into product properties. Field appropriateness was considered to be most important. Equipment weight and power consumption were to be kept at a minimum to ensure transportability and allow usage of car batteries as back-up power supply.

Unlike in water treatment or latrine construction [9], no standardized field fecal-sludge treatment plants are deployed by large humanitarian-aid organizations. Therefore, no treatment process cascade has been standardized. Thus, it was deemed highly important to enable the field laboratory to monitor a broad spectrum of different processes. A list of field-applicable treatment processes (Table 1) was compiled out of different literature sources [5,10–12]. Regarding these processes, a basic set of parameters for the field laboratory (Table 1) was established by a literature search [6,7,12–17] before onset of the development. In many countries, national regulations governing effluent qualities of fecal-sludge or wastewater treatment plants [15,16,18,19] do exist; however, guidelines regarding fecal-sludge treatment comparable to the WHO guidelines on water quality [20] on an international level are currently missing. The exception is the WHO guidelines on wastewater use in agriculture [17] and a drafted ISO norm for non-sewer sanitations systems [21]. While in the former public-health thresholds are established for the use of effluent streams in agriculture, minimum treatment efficiencies are indicated in the latter publication.

Parameter	Treatment Processes												
Turumeter	1	2	3	4	5	6	7	8	9	10	11	12	13
Ph-value	x	x	x	x	x	x	x	x	x	х	x	x	x
Temperature	х	х	х	х	х	х	х	х	х	х	x	х	х
E. coli/coliforms	х	х	х	х	х	х	х	х	х	х	x	х	х
Enterococci	х	х	х	х	х	х	х	х	х	х	х	х	х
Salmonella	х	х	х	х	х	х	х	х	х	х	x	х	х
Helminth eggs	х	х	х	х	х	х	х	х	х	х	х	х	х
Chemical Oxygen Demand	х	х			х	х	х			х	х	х	х
Biogas potential	х											х	х
Biogas composition	х											x	х
VFA/Alk titration	х		х		х							x	х
Sludge volume		х	х					х	х		х	х	х
Total solids	х	х	х			х	х	х	х	х	х	х	х
Ash	х	х	х			х	х	х	х	х	х	х	х
Soil moisture						x	x	x	x	х			
Ammonia	х	х		х		х				х			х
Nitrate		х					х						х
Potassium							x						
Phosphate		x					x						x
Total nitrogen (TN)		х		х		х	х			х			х
Total phosphate (TP)		x					x						x

Table 1. Parameters included, and processes considered in the field lab; parameters highlighted in grey were modified for field use.

1—Anaerobic digestion; 2—aerobic wastewater treatment; 3—lime addition; 4—urea addition; 5—lactic acid fermentation; 6—vermicomposting; 7—co-composting; 8—solar drying, 9—thermal drying and palletization; 10—black solider flies; 11—mechanical fecal-sludge (FS) treatment; 12—Imhoff tank; 13—cotreatment in waste-stabilization ponds.

The parameters used for process control strongly depend on the chosen treatment process. However, through the literature study a parameter set was developed that would allow minimum monitoring of a wide range of processes. The process-control equipment should allow the fecal-sludge treatment plant to be balanced (e.g., chemical oxygen demand, nitrogen, total solids). The estimation of treatment efficiency and subsequent comparison over time and with different plants is enabled by the calculation of influent and effluent freights. Further on, the process-control equipment is also used to characterize the effluent quality.

Analytical methods of field laboratory were chosen according to previously mentioned design criteria and the CATNAP principle defined by Duncan Mara [7]. CATNAP stands for "cheapest-available technology narrowly avoiding prosecution". While it was originally intended to be used in the construction of wastewater treatment plants, the mentality also applies to this field lab. For process control directly in the field during an emergency aid operation, a trade-off between ruggedness, ease of handling, and analytical precision can be made. For example, in the process monitoring of biogas plants for most parameters, ranges are given [14]. Thus, the needed precision in the field lab is to know if the analyte concentration is in a certain range. To reduce development time, the methods were based on well-established methods and only adapted to field conditions when needed.

In public-health monitoring of fecal-sludge treatment plants, bacteriological indicator organisms and helminth eggs are used. The analysis of the bacteriological indicator organism is discussed later on. The detection of helminth eggs are considered an increasingly important parameter for the public-health assessment of fecal-sludge treatment and subsequent reuse [22–24] Currently, helminth eggs are detected by microscopic identification. These methods can be considered challenging and expert training is needed. Digital-picture analysis software for automatic helminth-egg detection was developed by the University of Mexico [25]. The public availability of such software would ease the detection process and allow faster sample analytics. For the detection of helminth eggs in the field laboratory, MiniFlotac and FillFlotac and the corresponding methods developed by the University of Naples, Federico II, were used [26]. The public method was only modified by changing from an electrical to a hand-driven centrifuge and is thus not further elaborated in this study.

In any emergency-aid mission, any field lab needs to be set up and operational within the shortest time possible. To ensure the semi-independent operation of the lab support equipment (e.g., general lab equipment, personal protective equipment, and power converter with UPS function and solar panels to recharge batteries) was added and tested. Each of the modified analytical method (Table 1) was tested and adapted to field conditions (e.g., ruggedness, low power consumption, easy handling). To ensure functionality, each adapted method was cross-checked and compared to the results of the established, parent counterpart.

2. Materials and Methods

2.1. Samples

For the development of the analytical methodology of the field laboratory, the following different samples sources were used:

- Nonpathogenic Escherichia coli (E. coli) strain
- Ammonia sulphate solution from ammonia-extraction experiments
- Autoclaved garden soil spiked with E. coli
- Garden soil
- Pig manure of an Austrian pig-fattening farm
- Fecal sludge from a household septic tank

- Wastewater treatment plant influent and effluent of Tulln, Austria
- Effluent of a mesophilic lab-scale biogas plant

All samples were taken during the method-development work packages (November 2016–June 2017) of the Microbial Sludge Quality project. Sample characterization was not considered the main aim of the analytical work. In method development, the samples were used for comparison of results of the established and of the field laboratory method.

2.2. Bacteriology

One part of the public-health side is covered by the determination of bacteriological indicator organisms. The concept of fecal indicator organisms was developed in the late 19th century mainly to ensure microbiological safety of potable water [7]. These indicator organisms, which are excreted in large numbers with feces, in the best case are nonpathogenic, do not replicate in water, and easy to cultivate. For drinking water, absence of these organisms indicates a high chance of absence of pathogenic organisms. However, in fecal-sludge treatment, the analytical question is not detecting an absence of fecal indicator organisms but measuring their reduction through the treatment process. *E. coli* and coliforms are the oldest fecal indicator organism in use, but their viability has been discussed in the recent past, especially in its use in fecal-sludge and wastewater analytics [27]. Enterococci and *Salmonella* are two other fecal indicator organisms used in the public health assessment [28]. Enterococci are discussed as successor to E. coli due to their inability to grow in environmental water and higher resistance to disinfection methods [29]. Salmonella is of interest since most species are considered pathogenic. A plethora of different methods and analytical equipment is available for bacteriological analysis. As method, membrane filtration was chosen due to its relative precision, ease of handling, and its prevalence in water-quality-testing laboratories used in the humanitarian-aid community. In fecal sludge, soil, or wastewater, homogenization of samples is needed [30]. In fixed laboratories, a sterile blender or stomacher is used. Stomachers are heavy, expensive, and require several hundred watts of power. For the field lab, the stomacher was replaced with approximately 1000 stainless-steel cleaning beads in a bottle. The bottle was shaken for several minutes and the sludge was homogenized by the beads.

The bacteriological analytical method for detection of *E. coli*, Enterococcus, and *Salmonella* in the field lab was based on the U.K. Environmental Agency [31], the Standard Methods for the Examination of Water and Wastewater [32], and Sartorius [33] analytical methods for membrane filtration. A buffered solution (KH₂PO₄ and MgCl₂ $6 \times$ H₂O) was used for the dilution of sample. Stock solutions of both chemicals were separately prepared by weighing in 34 g KH₂PO₄/L (Carl Roth, Karlsruhe, Germany) and 81 g MgCl₂ $6 \times$ H₂O/L (Carl Roth, Karlsruhe, Germany), dissolving it in filtered (0.2 µm glass fiber membrane, Base Camp Pro 10 L, Katadyn, Wallisellen, Switzerland) tap water and autoclaving the bottles. The buffered, working solution was prepared from 1.25 mL KH₂PO₄ stock solution/L and 5.0 mL MgCl₂ $6 \times$ H₂O stock solution/L. The working solution was afterwards autoclaved, and stored dark and cool.

For homogenizations, the samples were diluted 1:10 with the dilution solution. In the established laboratory method, a stomacher (Maxicator, IUL, Barcelona, Spain) was used. A 10 mL sample was directly diluted in the stomacher bag with 90 mL of the dilution solution and afterwards homogenized (8 strokes/second and 240 s). For the field-lab method, the stomacher was replaced with 1000 stainless-steel cleaning beads (2 mm, Ecooe, Hong Kong, China). A 10 mL sample was diluted with a 90 mL dilution solution in an autoclaved 250 mL PP bottle (VWR, Radnor, PA, USA). The beads were placed in the bottle before autoclavation. To homogenize the sample, the bottle was manually shaken for 5 min, corresponding to 750 to 1000 shakes.

Both in the fixed- and field-laboratory method, the homogenized sample was further diluted by log steps (4 mL sample and 36 mL dilution solution) in autoclaved 50 mL PP bottles (VWR, Radnor, Pa, USA). Before membrane filtration, the filter holder (Witeg, Wertheim, Germany) was heat-sterilized using a gas-soldering torch. Membrane filtration was performed according to Sartorius guidelines [33]. For the

three analyzed bacteriological parameters, *E. coli* coliforms, Enterococcus, and *Salmonella*, nutrient plates (Sartorius, Göttingen, Germany) Endo, Azide, and Bismuth Sulfite, respectively, were used. Each sample was plated out in three successive dilution steps and in duplicates. Every 10 samples a blank water sample was filtrated. The nutrient plates were incubated for the specified time period at 36 ± 1 °C. The incubated nutrient plates were photographed using a commercial compact camera or smartphone and afterwards autoclaved. The colonies were counted on the pictures using Fiji (USA), open-source image-analysis software, and colony-forming units per mL.

For the field laboratory, two different incubators, a Hova Bator 1588 (GQF, Savannah, GA, USA) and a Cultura M (Merck Millipore, Burlington, MA, USA), were tested and compared. The Cultura M was further modified by installing a PC ventilator to ensure better temperature distribution. Both incubators were tested by a comparison of measured and set temperature in several different places.

2.3. Chemical Oxygen Demand (COD)

The oxygen demand is determined in two different ways and is an important parameter for process control and effluent quality [6]. The total chemical oxidizable content of a sample is represented by the COD and indicates the energy content or organic pollution [14]. For the determination of the biological oxygen demand (BOD), aerobic micro-organisms are used to degrade the sample. Their oxygen consumption is used to estimate the biological degradability of the sample. While BOD would be of higher interest for biological treatment processes, in the field laboratory only COD is determined. COD determination is considerably faster and itself of a higher precision, especially when fecal sludge is analyzed. In fecal sludge, several noncarbonaceous chemicals are often present in an unoxidized form. During a BOD determination, these chemicals increase the total oxygen consumption and thus bias the result [6]. For COD determination, a digestion system is needed. The samples are digested using sulphuric acid and heat. Laboratories customarily use electric digestion systems. These consume several hundred watts of electrical power, and are heavy and expensive. For the field lab a digestion method was developed employing a sand bath in a cooking pot placed on a gas stove.

For the determination of COD, a photometric cuvette test was used. During the laboratory development, an LCK 014 and 114 test set, a DR2800 photometer, and a HT200S digestion block, all from Hach (Loveland, CO, USA), were used.

For field use, a sand bath (Figure 1b) digestion setup was developed and tested. The sand bath consisted of a 2 L metal cooking pot with a digital temperature indicator fixed to it. The temperature indicator was fixed at the height of the maximum immersion depth of the photometric cuvettes (Figure 1a). The sand bath was heated on a gas stove. The digestion method was developed to mimic the Hach (USA) high-temperature method, which uses a digestion temperature of 170 °C and a time of 20 min. For the field method, a temperature range of 160 to 180 °C for digestion was established and tested. Due to heat stored in the sand, the temperature would increase after the heat source was shut off. Before the first digestion of samples, a dry run without samples to establish the right shut-off point was needed to be done. The sand bath was heated on a gas stove. The cuvettes were prepared according to the manufacturer's instructions. All samples used for method development were analyzed in duplicate. At a sand temperature of approximately 100 °C, the cuvettes were placed in the sand bath. At a beforehand-determined point, commonly 160 °C, the heat source was shut off and the temperature increased but stayed in the temperature band. After 20 min, the cuvettes were removed from the sand bath and put aside to cool. Before measurement, according to the Hach

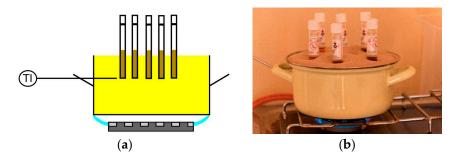


Figure 1. Gas stove sand bath digestion system. (**a**) Scheme of the digestion system; (**b**) picture of the system during a field test.

2.4. Volatile Fatty Acid (VFA)/Bicarbonate Alkalinity (Alk) Titration

For biogas plants, the ratio of VFAs to the Alk is powerful process stability indicator [14]. Inhibitions in biogas plants are often accompanied by an increase in the VFA concentration. The applied method uses an acid titration and is considered routine analysis for biogas plants. In the established laboratory method, a fully automated titration device is used. Automatic titrators are quite expensive and need a stable (110 or 230 V) power supply. For the field laboratory, a similar device was constructed out of Vernier parts. Most of the Vernier equipment is also used for the analysis of different parameters, operates on batteries and is less expensive.

VFAs and Alk were measured in both lab setups by titration. In the fixed laboratory an autotitrator (Titrino 721 NET, Metrohm, Herisau, Switzerland) was used and compared to the field-lab method using a pH sensor (ph-bta), a drop counter (VDC-BTD), and a LabQuest Stream data collector, all from Vernier (Beaverton, OR, USA). The drop counter's original tip was replaced with an injection cannula to decrease droplet size. 1 mL of sample, diluted to 50 mL with reverse-osmosis water, was titrated with 0.1 M HCl to the pH point 5.0 and a pH end point of 4.5 following a protocol provided by the manufacturer. All samples were determined in triplicates. The formula provided by Drosg [14] was used for calculation of results.

2.5. Total Solids (TS) Determination

TS are determined by drying a sample and differential weighing. Two different determination methods are used in laboratories. The first method, described in most handbooks calls for drying the sample overnight at 105 °C [32]. Customarily, electrical-drying ovens are used. These are large, heavy, expensive, and consume a lot of power. Infrared moisture analyzers are used in the second common method. These analyzers combine a drying element with a scale. A sample is placed in a tin crucible on the scale and dried at a higher temperature (often 120 °C) in place. The scale automatically controls the drying process and calculates the total solids content. These moisture analyzers are expensive, fragile, and, due to use of electronics, rely on stable power supply. For the field laboratory a camping baking oven placed on a gas stove was used instead of an electric drying oven. This system is cheaper, lighter, and more rugged than both alternatives.

Total solids in the fixed laboratory were determined by differential weighing after drying at 105 °C over night in an Heraeus drying oven (Fisher Scientific, Hampton, NH, USA). In the field lab a camping baking oven (Coleman, Wichita, KS, USA) on a gas stove was used. To reduce drying time the temperature was increased to 120–140 °C. The temperature was manually regulated by adjusting the gas flame. The samples were determined in duplicate.

2.6. Ammonia Determination

Test strips offer the possibility to analyze a wide range of different parameters at a comparatively low price per test. However, two challenges were found when used with fecal sludge or wastewater. Most test strips were designed to analyze water samples. Fecal sludge and wastewater have a higher particle density and often a distinct color—both can bias the test result. To reduce the particle load, the samples were centrifuged and only the supernatant analyzed. Test strips are normally assessed with the operator's eyesight. Thus, a human-error element is introduced. Test-strip manufacturers have recognized this problem and developed test-strip photometers. While they are light and operate on batteries, these photometers are expensive. The Dutch Akvo foundation has developed a method that allows assessment of test strips using a color card and a smartphone app [34]. In the field lab the methodology was adapted to fecal sludge. In this study a focus was laid on ammonia test strips. Their results were compared with two established methods (photometric tests and water-vapor distillation).

Ammonia concentration in the field laboratory was determined using Quantofix test strips (Macherey-Nagel, Düren, Germany) in combination with Akvo Caddisfly color cards and smartphone app (Akvo foundation, Amsterdam, The Netherlands). Due to the coloration of fecal-sludge samples were centrifuged (1500 rpm, 2 min, Hettich hand centrifuge, Kirchlengern, Germany) and, if necessary, diluted with reverse-osmosis water.

The field-laboratory method was compared to two ammonia-determination methods. One sample set was analyzed using a Büchi distillation/titration unit (K370, Büchi, Flawil Switzerland). The second sample set was analyzed a photometric method based on indophenol formation with sodium salicylate. The method follows the protocol described in the German standard methods (DIN 38406/5) but was downsized to the ml scale to allow the use of 24-well microtiter plates (Falcon, Cornig, NY, USA) and photometric analyses in a plate reader (Infinite M200 Pro, Tecan, Männedorf, Switzerland). Samples were centrifuged (12,500 rpm 15 min; CS-15 Beckman Coulter, Brea, CA, USA), the supernatant was used for further analysis. Samples from the scrubber were analyzed directly without pretreatment. Each sample was diluted in three different ratios, and the average of values within the calibration range was taken as the result. All ammonia determinations, with either the field method or the laboratory methods, were conducted in duplicate.

3. Results

3.1. Bacteriology

For precise bacteriological results, stable incubation temperatures are needed. For the incubation of all indicator organisms used in the field laboratory, a temperature of 36 ± 1 °C was required [30]. Two different commercially available field incubators were tested (Table 2). The Cultura Mini, due to previous usage within the Austrian Red Cross, was acquired and tested first. After analysis of the first test results, the incubator was modified by installing a small PC fan to improve the temperature distribution. While through this modification the required temperature range was reached, it was decided to search for a commercial available product with a different design. The Hova Bator Genesis was suggested by a water-quality-testing manual [35]. This incubator was originally intended for incubation of poultry eggs, which requires precise temperature control. It was already equipped with a fan, better temperature control system, and operated on a 12 V power supply.

Table 2. Temp	erature compai	rison of different	tested incubators.
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	Cultura Mini	Cultura Mini Mod.	Hova Bator Genesis 1588
Set temperature (°C)	37.0	32.0	36.0
Average temperature (°C)	38.8	31.2	36.1
Deviation from set temperature (°C)	1.8	0.8	0.1
Standard deviation (°C)	1.9	0.8	0.1
Time until temperature stable (min)	260	180	10

For bacteriological analysis of fecal-sludge sample homogenization is considered highly important. A laboratory stomacher was compared to the stainless-steel homogenization field method with different sample matrices (Figure 2a and Table A1). The results displayed are the average of multiple analysis (Tables A2 and A3). For liquid-sludge samples, fecal sludge from a septic tank and pig manure from

a farm storage tank were analyzed. To simulate soil and compost samples, garden soil was autoclaved and dried and seeded with a known *E. coli* concentration (log 5 CFU/mL). On average, 5.9 ± 0.1 log CFU/mL was found. The recovery rate for all different sample matrices ranged between 67% and 133%.

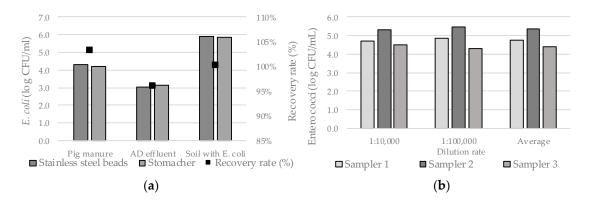


Figure 2. Results of bacteriological method development. (a) Homogenization experiments and (b) differences through sampling.

In a second set of experiments (Figure 2b and Table A4), the effects of sampling were investigated. A 60 L barrel was filled with fecal sludge and stirred for several minutes before it was sampled by three laboratory technicians. While the analytical results were consistent between the dilutions steps of a sampler, the averaged results of each sampler differed by up to one log unit. Enterococci concentration of 4.4 ± 0.1 to 4.8 ± 0.1 log CFU/mL was reported by sampler 1 and 3. Concentrations of one log unit higher (5.4 ± 0.1) were reported by sampler 2 (Table A5).

3.2. Chemical Oxygen Demand Determindation

A sand bath on a gas stove was used as the sample digestion system. To estimate the shut-off temperature of the gas stove, several trials were conducted (Figure 3b). The gas stove was shut off at 160 °C. In all experiments, the temperature stayed in the required band for over 20 min.

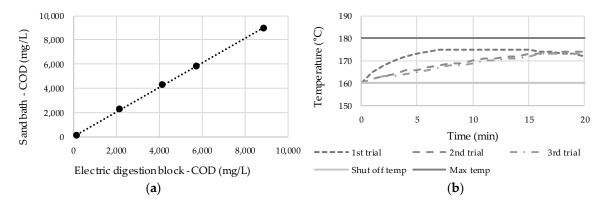


Figure 3. Modification of the Chemical Oxygen Demand (COD) method (**a**) comparison between electric digestion block and sand bath; (**b**) temperature curves for the sand bath digestion system.

Wastewater, manure, and fecal-sludge samples with different COD concentrations were measured using both digestions systems and the results compared to each other (Figure 3a and Table A6). The measured COD ranged from 160 to 9.070 mg/L COD and a recovery rate between 95%–106% was calculated. Due to the range limitation of the photometric COD tests, two different test sets had to be used.

3.3. Volatile Fatty Acid to Alkalinity Titration

For the method development, pig manure and anaerobic digestion (AD) effluent samples were analyzed with the autotitrator and the field set up. In Figure 4a, the results of the VFA titration and in Figure 4b the results of the VFA/Alk are shown. The raw data are shown in Tables A7–A9. The recovery rate for VFA and the ratio ranged between 48% to 190% and 46% to 157%, respectively.

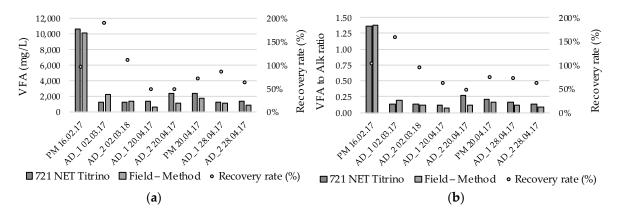


Figure 4. Modification of Volatile Fatty Acid (VFA)/Bicarbonate Alkalinity (Alk) titration; comparisons of (**a**) VFA results and (**b**) the complete VFA/Alk ratio PM—pig manure; AD—anaerobic digestor effluent.

3.4. Total Solids Determination

For the evaluation of the TS methodology, fecal sludge from a household septic tank and soil was used. The results (Tables 3 and A10) represent the average of multiple determinations. The fecal-sludge sample was take from the septic tank of a family house and stored in a 60 L barrel. The TS samples were taken in the course of a month.

Table 3. Modification of the Total Solids (TS) method; comparison of camping baking oven and electrical oven.

	Sampling Point 1	Sampling Point 2	Sampling Point 3	Soil
Camping oven (g/kg)	71.5 ± 3.2	71.3 ± 1.1	70.5 ± 1.0	429.7
Lab drying oven (g/kg)	70.6 ± 0.4	73.2 ± 1.4	72.5 ± 0.9	424.1
Recovery (%)	101%	97%	97%	101%

3.5. Ammonia Determination

For the first tests of the ammonia–nitrogen (NH₄-N) test strips, samples from an ammonia-stripping experiment were used. The samples were clear diluted sulphuric acid with an increasing ammonia concentration. The test-strip results were compared with photometric tests (Figure 5a and Table A11). A general trend of higher results reported by the test strips was observed. The recovery rate was averaged at 160%. A second set of tests (Figure 5b and Table A12) was conducted with real samples (pig manure, AD effluent, fecal sludge). The previously observed trend of higher results was not repeated. A recovery rate of 59% to 105% was reported.

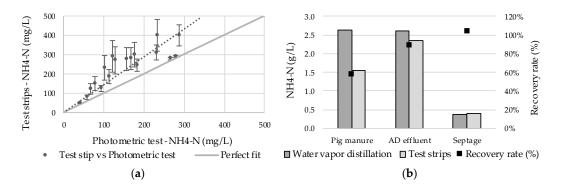


Figure 5. Ammonium–nitrogen (NH₄-N) determination: comparison of test strips with (**a**) photometric tests with watery samples and (**b**) water-vapor distillation with sludges.

4. Discussion

4.1. Analytical Methods Modified for Field Use

4.1.1. Bacteriology

By using the stainless-steel bead methodology instead of a stomacher, no significant differences in homogenization were noticed. During the bacteriological analysis of sterilized soil spiked with *E. coli*, a significantly lower standard deviation was found than in similar research [36]. The difference in the bacteriological results between samplers, with a standard deviation of 0.4 log units, was found to be in range with results presented by the literature [5,37].

Manual digital colony counting using an image-processing system sped up the process and reduced the contact time with possibly contaminated equipment. Freeware colony-counting software was tested, but due to a low colony-recognition percentage, it was found to be unhelpful. However, when these systems become fully operational, it is estimated that bacteriological analysis will be sped up. Membrane filtration was chosen due to its wide spread use in water analysis with humanitarian-aid organizations. However, fecal-sludge analytics compared to water analytics is significantly more complex. For future iterations of the laboratory, it might be prudent to develop an easier bacteriological methodology.

4.1.2. Chemical Oxygen Demand

The results from the sand-bath digestion system correlated ($R^2 = 0.999$) with the results of the electric digestion system. Compared to the electric digestion system, the field method is slower and more difficult to handle; however, it is cheaper and does not require electricity. If the sand-bath digestion is used, the cuvettes need to be wiped off to remove residual sand particles before measurement in a photometer. To enable the usage of the sand-bath digestion system, the high-temperature digestion methodology developed by Hach must be supported by the used brand of cuvette tests. While the focus of the experiments was laid on COD determination, total nitrogen and total phosphate also require sample digestion and could use the sand bath.

4.1.3. Volatile Fatty Acid and Alkalinity Titration

The VFA/Alk ration, determined by titration, is an important process parameter for anaerobic digestion plants. It indicates the process stability regarding feeding regime and inhibition of the acetogenisis and methanogenesis. Using the field method, generally lower results were found in comparison to the autotitrator. The different results in the titration can be attributed to different pH electrodes, inhomogeneous samples, and the more exact dosage system of the autotitrator. However, these differences are not as significant, because the aim of the VFA/Alk ratio measurement is the detection of a change or drift in the ratio. Further on, differences, e.g., in feed compositions and

reactor management, make a realistic comparison between different anaerobic digestion plants not feasible [14].

4.1.4. Total Solids

Due to the manual control of the temperature of the camping baking oven, the drying time had to be reduced by increasing the temperature. The chosen temperature of 140 °C was copied from a Sartorius infrared moisture used for quick analysis for wastewater and anaerobic digestion samples. For the field method it was broadened to 120–140 °C. A loss of volatile compounds due to the higher drying temperature was not observed during the experiments.

4.1.5. Ammonia Determination

Test strips in general, and especially the tested ammonia test strip, were developed for water testing and not with fecal sludge as matrix in mind. Some of the matrix effects were countered by adaptions in the analytical method, e.g., analyzing centrifuged sludge. Therefore, lower analytical precision was expected and found. However, similar problems are encountered with most photometric cuvette tests used in the process control of state-of-the-art anaerobic digestion plants.

As the test strips are to be used for process control in a field fecal sludge treatment plant in a humanitarian aid setting, a lower analytical precision was found acceptable. In the process control of most treatment processes the values are allowed in a certain range (e.g., for anaerobic digestion plants [14]). The experiments were focused on ammonium; however, nitrate, nitrite, phosphate, and potassium are as well determined with test strips.

4.1.6. Overall Considerations on Modified Methods

While the modified methods were analytically compared to their respective laboratory counter parts, the field methods were not analytically validated. As already discussed above, some of the analytical results from both sets of methods differ significantly (mainly test strips, VFA/Alk titration). However, even these methods can be considered viable for field-process control of fecal-sludge treatment plants, since in process control thresholds are expressed in ranges and trends are monitored. More research is needed to validate each of the modified analytical methods.

4.2. Design Creiteria

For the successful development of the field laboratory, the previously described design criteria have to be met. The design criterion "Appropriateness" is defined by obtaining comparable analytical results of a fixed, modern laboratory. Modifications of methods like bacteriology or COD digestion have yielded highly comparable results. While the results of some of the modified methods (e.g., ammonia or VFA/Alk) are not as exact as their respective originals, they still fulfill the aim of enabling process control of a fecal-sludge treatment plant directly in the field.

By "Applicability", the operability of the laboratory in the field is meant. In short, the laboratory must work in the field. Some methods were required to be adapted to field conditions. The main reasons for modifications were equipment weight and power consumption. Through these changes, these methods have become more labor-intensive and rely heavily on manual control of previously automated equipment. It is estimated that in comparison to a fixed laboratory, the field laboratory will have a lower sample throughput per day. While more labor-intensive, the modified methods have not necessarily become more complicated. However, skilled and well-trained technicians are needed to operate any laboratory, especially a field laboratory. Besides the redevelopment of analytical methodology, the aim of the project was the development of a whole field laboratory. Therefore, support equipment was added. This equipment allows immediate semi-operation of the laboratory in the field.

For humanitarian-aid organizations, the main target group "Affordability" is of high importance. Even during humanitarian-aid, operations budgets are often constricted. The product choices were guided by the CATNAP principle [7]. Through the adaption of analytical methods to field conditions, a cost reduction in comparison to regular laboratory equipment was reached. The first example is the electrical laboratory drying costs—approximately \pounds 1000—while the camping baking oven is around 65 \pounds . The second example is the COD digestion block, which costs between \pounds 1000–2500. The sand-bath sample digestion costs below 100 \pounds .

"Mobility" is a crucial attribute for any humanitarian-aid equipment. It was defined by the project team that the laboratory has to fit in a Toyota Landcruiser [38], which can be considered the universal vehicle of humanitarian aid. While no Landcruiser was available, the laboratory nicely fit into the trunk of a VW transporter. The whole field laboratory with consumables for 100 samples, deployed to Malawi for the filed trail, not covered in this study, weighed approximately 220 kg and had a shipping volume below 2 m³.

5. Conclusions

Usage of the field lab should provide direly needed information on the effluent characteristics of field-treatment plants on site and close in time. This information will allow treatment-plant operators better control of their treatment process, thus ensuring better public health and environmental protection in humanitarian aid. To reach this goal, several analytical methods were modified for field use and compared the original methods. Of the modified methods, the bacteriological analysis, COD, and total solids determination provided highly comparable results. The results of titration of VFA/Alk ratio and ammonia determination were not as well comparable. However, the obtained results were considered acceptable for the purpose of field-process monitoring of fecal-sludge treatment plants.

As the work presented in this study is the first version of a field laboratory for the process and public-health monitoring of fecal-sludge treatment plants, the researchers acknowledge that room for improvement in the laboratory exist.

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Appendix A

Source	Type of Homogenization	Colonies	Dilution Rate	E. coli (log CFU/mL)
Pig manure	Stainless steel beads	43	10,000	4.3
Pig manure	Stainless steel beads	68	10,000	4.5
Pig manure	Stainless steel beads	3	100,000	4.2
Pig manure	Stainless steel beads	4	100,000	4.3
Pig manure	Stomacher	52	10,000	4.3
Pig manure	Stomacher	38	10,000	4.1
Pig manure	Stomacher	3	100,000	4.0
Pig manure	Stomacher	5	100,000	4.3
AD effluent	Stomacher	49	1000	3.2
AD effluent	Stomacher	35	1000	3.1
AD effluent	Stomacher	3	10,000	3.0
AD effluent	Stomacher	6	10,000	3.3
AD effluent	Stainless steel beads	33	1000	3.0
AD effluent	Stainless steel beads	28	1000	3.1

Table A1. Raw data from bacteriological homogenization experiments.

Source	Type of Homogenization	Colonies	Dilution Rate	E. coli (log CFU/mL)
AD effluent	Stainless steel beads	2	10,000	2.8
AD effluent	Stainless steel beads	4	10,000	3.1
Soil with E. coli	Stomacher	206	100,000	5.8
Soil with E. coli	Stomacher	196	100,000	5.8
Soil with E. coli	Stomacher	25	1,000,000	5.9
Soil with E. coli	Stomacher	23	1,000,000	5.9
Soil with E. coli	Stainless steel beads	138	100,000	5.7
Soil with E. coli	Stainless steel beads	209	100,000	5.8
Soil with E. coli	Stainless steel beads	220	100,000	5.9
Soil with E. coli	Stainless steel beads	213	100,000	5.9
Soil with E. coli	Stainless steel beads	34	1,000,000	6.1
Soil with E. coli	Stainless steel beads	40	1,000,000	6.1
Soil with E. coli	Stainless steel beads	20	1,000,000	5.8
Soil with E. coli	Stainless steel beads	25	1,000,000	5.9

Table A1. Cont.

Table A2. Averages of homogenization experiments.

Average (log CFU/mL)	Pig Manure	AD Effluent	Soil with E. coli
Stainless steel beads	4.3	3.0	5.9
Stomacher	4.2	3.2	5.7
Recovery rate (%)	104%	96%	100%

 Table A3. Standard deviation of the homogenization experiments.

SD (log CFU/mL)	Pig Manure	AD Effluent	Soil with E. coli
Stainless steel beads	0.1	0.1	0.1
Stomacher	0.1	0.1	0.1

Table A4. Raw data from the differences in sampling experiments.

Sampled by	Colonies Counted	Dilution Rate	Enterococci (log CFU/mL)
Sampler 1	127	10,000	4.7
Sampler 1	137	10,000	4.7
Sampler 1	22	100,000	4.9
Sampler 1	20	100,000	4.8
Sampler 2	478	10,000	5.2
Sampler 2	74	100,000	5.4
Sampler 2	83	100,000	5.4
Sampler 3	83	10,000	4.5
Sampler 3	92	10,000	4.5
Sampler 3	6	100,000	4.3
Sampler 3	6	100,000	4.3

Table A5. Averages and standard deviation of the differences in sampling experiments.

(log CFU/mL)	1:10,000	1:100,000	Average	SD
Sampler 1	4.7	4.8	4.8	0.1
Sampler 2	5.3	5.4	5.4	0.1
Sampler 3	4.5	4.3	4.4	0.1
All Samplers	4.8	4.9	4.8	0.4

	Labo	ratory Me	thod		Field Met		
Test (COD mg O ₂ /L)	1	2	Average	1	2	Average	Recovery Rate (%)
1	5750	5980	5870	5950	5710	5830	99%
2	2150	2160	2160	2290	2280	2290	106%
3	8730	8950	8840	9070	8950	9010	102%
4	164	166	170	162	150	160	94%
5	4220	4100	4160	4170	4450	4310	104%

Table A6. COD measurement raw data.

 Table A7. VFA titration results, PM—pig manure; AD—anaerobic digestion effluent.

VFA (mg/L)	721 NET Titrino	Field—Method	Recovery Rate (%)
PM 16.02.17	10,600	10,200	96%
AD_1 02.03.17	1200	2290	190%
AD_2 02.03.18	1290	1410	109%
AD_1 20.04.17	1350	660	48%
AD_2 20.04.17	2350	1120	48%
PM 20.04.17	2380	1700	71%
AD_1 28.04.17	1290	1090	85%
AD_2 28.04.17	1420	890	63%

 Table A8. Alkalinity titration results, PM—pig manure; AD—anaerobic digestion effluent.

Alk (mg/L)	721 NET Titrino	Field—Method	Recovery (%)
PM 16.02.17	7800	7380	95%
AD_1 02.03.17	9600	11,610	121%
AD_2 02.03.18	10,120	11,790	116%
AD_1 20.04.17	11,310	8930	79%
AD_2 20.04.17	8770	9110	104%
PM 20.04.17	11,080	10,720	97%
AD_1 28.04.17	8130	9770	120%
AD_2 28.04.17	10410	10700	103%

 Table A9. VFA to alkalinity ratio, PM—pig manure; AD—anaerobic digestion effluent.

VFA/Alk	721 NET Titrino	Field—Method	Recovery Rate (%)
PM 16.02.17	1.36	1.38	101%
AD_1 02.03.17	0.13	0.20	157%
AD_2 02.03.18	0.13	0.12	94%
AD_1 20.04.17	0.12	0.07	61%
AD_2 20.04.17	0.27	0.12	46%
PM 20.04.17	0.21	0.16	74%
AD_1 28.04.17	0.16	0.11	70%
AD_2 28.04.17	0.14	0.08	61%

	Camping Oven (g/kg)	Electric Drying Oven (g/kg)
FS Sample 1	69.0	70.9
FS Sample 1	68.8	70.3
FS Sample 1	75.4	-
FS Sample 1	72.7	-
FS Sample 2	69.9	72.3
FS Sample 2	72.2	72.4
FS Sample 2	70.5	74.8
FS Sample 2	70.7	-
FS Sample 2	71.9	-
FS Sample 2	72.8	-
FS Sample 3	70.8	72.7
FS Sample 3	70.6	72.8
FS Sample 3	71.1	72.5
FS Sample 3	71.8	73.4
FS Sample 3	69.2	72.6
FS Sample 3	69.4	70.8
Soil	440.0	448.3
Soil	419.4	400.0

Table A10. Raw data of the total solid determination experiments.

Table A11. Raw data photometric testing vs. te	est strips.
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Test	Photometric Test (mg NH4-N/L)	Test Strip (mg NH4-N/L)	Recovery Rate (%)
1	58	80	137%
2	113	185	164%
3	167	280	167%
4	230	310	135%
5	278	290	104%
6	94	125	133%
7	175	300	171%
8	266	280	105%
9	41	47.5	115%
10	66	120	181%
11	101	230	227%
12	129	270	210%
13	156	275	177%
14	78	150	193%
15	122	290	238%
16	183	245	134%
17	233	400	172%
18	288	400	139%

Table A12. Comparison water-vapor distillation vs. test strips.

	Water Vapor Distillation (g NH4-N/L)	Test Strips (g NH4-N/L)	Recovery Rate (%)
Pig manure	2.62	1.55	59%
AD effluent	2.62	2.35	90%
Septage	0.37	0.39	105%

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